PATENT SPECIFICATION

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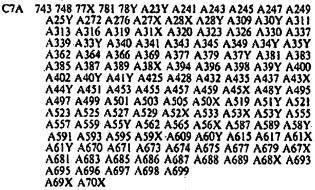
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(54) WEAR-RESISTANT CAST-IRON ALLOY

GOETZEWERKE FRIED-GOETZE AKTIENGESELL-SCHAFT, a Body Corporate organised and existing under the laws of the Federal Republic of Germany, of Bürgermeister-Schmidt-Strasse 17, 5763 Burscheid, Ger-many, do hereby declare the invention, for which we pray that a patent may be granted to us, and the method by which it is to be performed, to be particularly described in and by the following statement:-

The present invention relates to a wearresistant cast from alloy suitable for the construction of machine parts subject to high frictional stresses.

Machine elements subjected to friction are strongly stressed both with regard to wear and thermally, so that particularly high demands have to be made on their materials. Certain machine elements, such as the piston rings of internal combustion engines and the sealing strips of rotary piston engines, are furthermore subjected to particularly heavy stresses. Experience has shown that only very expensive materials of complicated manufacture withstand such high stresses. Usually, these materials are sintered metal carbides. to which very specific alloying elements have bren added.

The sorts of cast iron so far tested, however, cannot be used for these highly stressed mochine parts. It is known that the wear

resistance of east iron can be increased by the addition of alloying elements. On solidification of the cast iron, however, these elements form relatively coarse grains and very hard carbides, which then cause damage, accompanied by scering, to the contacting surfaces. At the same time, carbide formation uses up the greater part of the carbon, so that these alloys do not contain in their structure. the necessary graphite for emergency run-ning of machine elements. Furthermore, these materials are so brittle that they are unable to withstand mechanical stresses and therefore break.

In accordance with the present invention there is provided a wear-resistant cast iron alloy, suitable for the construction of machine parts subject to high frictional stresses, the alloy containing

1.5 to 4.0% by weight of carbon 1.5 to 6.0% by weight of silicon less than 0.2% by weight of sulphur less than 2.5% by weight of phosphorus 1.0 to 7.0% by weight of copper 0.4 to 3.2% by weight of nickel and/or tledoo

0.1 to 1.8% by weight of tin and/or antimony

0.1 to 4.0% by weight of molybdenum 0.1 to 4.0% by weight of tangsten 0.05 to 2.5% by weight of manganese



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	0.3 to 2.5% by weight of chromium 0.3 to 4.0% by weight of vanadium 0 to 2.0% by weight of titanium 0.1 to 4.0% by weight of niobium and/or	0.9% by weight manganese 0.4% by weight chromium 1.5% by weight vanadium 0.2% by weight titanium	65
5	0.1 to 2.0% by weight of aluminium	0.7% by weight nlobium 0.01% by weight boron 0.22% by weight aluminium	70
10	and the rest iron except for atmospheric nitrogen combined with the metals as a result of melting and heat treatment. The cast iron alloys in accordance with the invention display uncombined carbon as	and the rest iron. After inoculation with one of the usual in- oculants, sealing strips for rotary piston engines were cast from the melt using the	
15	lamellar and primarily nodular precipientes. There are also present however a large number of carbides in a very fine crystalline precipitated form.	sand mould casting process, the dimensions of the strips being 61.03×8.3×4.95 mm. They were then annealed for one hour at 850°C, quenched in an oil bath at room temperature	75
20	The sum of the elements carbon and silicon in the alloys in accordance with the invention is equal to or greater than 3% by weight and the ratio of silicon to carbon is preferable equal to a greater than the sum of the s	and tempered for one hour at 350°C. The scaling strips thus made had an HV 5 hardness of 644 to 713 kg/mm². In test runs, the scaling strips showed very good	80
20	ably equal to or greater than one. The sum of the elements molybdenum, tungsten and manganese should preferably be between 0.2 and 10% while the sum of the elements chromium, vanudium, tantalum and niobium	wear resistance, while the trochoidal running surfaces were only slightly affected. Figures 1 to 4 show photomicrographs of the east-iron alloy of the example. Figure 1 is the unerched specimen at a	85
25	should preferably be between 1 and 10%. In addition, it has been found that for refining the form of the individual structural	magnification of ×100, showing the graphite in lamellar to nodular form. Figure 2 is the unetched specimen at a	90
30	constituents, more particularly that of the graphite, and the nitrides (when present), the clements boron, bismuth, zirconium, magnesium and/or the rare-earth metals may be	magnification of ×500, showing in addition to the dark graphite precipitates, the finely crystalline carbide constituents as light areas with a dark edge.	
35	added. Their total concentration should not, however, exceed the value of 0.5 percent by weight. By heat treatment above 700°C, followed	Figure 3 shows a specimen etched with HNO ₂ at a magnification of ×500 which shows, in addition to the graphite precipitates and the crystalline carbide constituents, the	95
••	by quenching for example in air or a saft bath to a temperature of below 500°C, and subsequent tempering up to a temperature of 700°C, wear resistance and compatibility with	bainitic to martensitic structure. Figure 4 shows the phosphide eutectic, deeply etched, at a magnification of ×20.	100
40	the counter-material are greatly increased. The alloys according to the invention have a bainitie to martensitic basic structure. The graphite precipientes are lamellar to nodular,	WHAT WE CLAIM IS:— 1. A wear resistant cast iron alloy, suitable for the construction of machine parts subject	
45	the carbide precipitates are punctiform to spherical. The hardness of this material at HV 5 lies at 550 to 920 kg/mm ² . The material is not brittle and cust scaling strips	to high frictional stresses, the alloy containing 1.5 to 4.0% by weight of carbon	105
50	for rotary piston engines are wear resistance and in test runs exhibit very good wear resistance with the trochoidal surface of the rotary piston engine. The embodiment example describes one of	1.5 to 6.0% by weight of silicon less than 0.2% by weight of sulphur less than 2.5% by weight of phosphorus 1.0 to 7.0% by weight of copper 0.4 to 3.2% by weight of nickel and/or	110
55	the cast-iron alloys according to the invention. The cast-iron melt camprises the elements	0.1 to 1.8% by weight of tin and/or anti-	115
<i></i>	2.2% by weight carbon 3.9% by weight silicon 0.9% by weight phosphorus 0.08% by weight sulphur 1.4% by weight copper	0.1 to 4.0% by weight of molybdenum 0.1 to 4.0% by weight of tungsren 0.05 to 2.5% by weight of manganese 0.3 to 2.5% by weight of chromium	150
60	0.6% by weight nickel 0.2% by weight tin 1.5% by weight molybdenum 3.4% by weight tangsten	0.3 to 4.0% by weight of vanadium 0 to 2.0% by weight of utanium 0.1 to 4.0% by weight of niobium and/or cantalum 0.1 to 2.0% by weight of aluminium	120

and the rest iron except for atmospheric nitrogen combined with the metals as a result of melting and heat treatment

of melting and heat treatment.

2. An alloy as claimed in Claim 1 modified by the addition of up to 0.5% by weight in total of one or more of the elements boron, bismuch, magnesium, zirconium and rare earth metals.

3. An alloy as claimed in Claim 1 or 2

which has been subjected to heat treatment by annealing above 700°C, quenching to below 500°C and then tempering up to a temperature of 700°C.

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COMPLETE SPECIFICATION

1 SHEET

This drawing is a reproduction of the Original on a reduced scale

F16.1



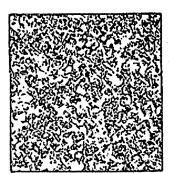




FIG. 3

F16. 4

